

PATENT

## LINEAR VOICE COIL ACTUATOR WITH COMPENSATING COILS

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Related Applications

- 5           The present application claims priority under 35 U.S.C. § 119(e) from provisional application number 60/192,999 filed March 28, 2000.

Technical Field

- The present invention is directed generally to linear actuators, and more particularly to compensating magnetic flux generated by the  
10       current in the moving coil of voice coil actuators.

Background Art

- Voice coil actuators are electromagnetic devices which provide force proportional to current applied to a coil. United States Patent  
15       number 5,677,963, assigned to the assignee of the present application, is a example of such voice coil actuators, and incorporated by reference herein in its entirety.

- Different configurations of linear voice coil actuators can provide different shapes of the Force vs. Stroke curves. However, these shapes cannot be changed without increasing the power level in the moving  
20       coil. But even this measure achieves only limited results due to a given distribution of the primary magnetic field and the armature reaction.

- In a servo system, it may be necessary to maintain constant force or constant speed within a certain stroke. United States Patent number 5,177,383, entitled "Voice coil motor," discloses coils with shorted turns  
25       employed in an attempt to achieve such characteristics. Because the turns in those coils are shorted, however, current in those turns cannot be adjusted when the moving coil moves from one position to another.

Summary of the Invention

- In accordance with the present invention, one or more separate  
30       compensating coils are employed to alter the distribution of the magnetic flux density in the air gap to produce a constant force

throughout as much stroke as possible. Current in the separate compensating coils can be adjusted with the stroke using separate power supplies and a position feedback.

These and other features of the present invention will be more readily appreciated upon consideration of the following detailed description and accompanying drawings.

Description of the Drawings

Fig. 1 is a simplified cross section of a closed ended linear voice coil actuator embodiment of the present invention.

Fig. 2 is a simplified cross section of an open-ended linear voice coil actuator embodiment of the present invention.

Figs. 3 and 4 depict required magneto-motive force in Ampere-turns vs. stroke for a given constant value of the output force of compensating coils positioned in at the ends of the magnets, and around the core, respectively, in accordance with the present invention.

Figs. 5 and 6 depict Force vs. Stroke characteristics with two different types of compensating coils in accordance with the present invention.

Fig. 7 is a simplified functional block diagram illustrating the connection of the compensating coils to separate power supplies with the value of the compensating current to the compensating coils being controlled as a function of stroke in accordance with the present invention.

Detailed Description

Referring to Fig. 1, in accordance with the present invention, compensation coils, for example 10-A, can be wound directly around the core 12; or compensation coils, for example 10-B and 10-C, can be located in the cavities, for example cavities 14 and 16, between the magnets 18 and inside surfaces 20 of the field blank 22 of the actuator. Compensation coils 10-A, 10-B and 10-C can be used in closed-ended

actuators, as shown in Fig. 1, as well as open-ended actuators, as shown in Fig. 2.

As can be seen in the closed-ended embodiment of the invention illustrated in Fig. 1, a core compensating coil 10-A is provided. A permanent magnet 18 is positioned with respect to the core 12 so that the longitudinal axis of the permanent magnet 18 is substantially parallel with the axis of the core 12. A field blank 22 made from soft magnetic material is used to form a magnetic circuit between the ends of core 12 and around permanent magnet 18.

10 A voice coil actuator in accordance with the present invention can have a variety of shapes, including a rectangular configuration and a cylindrical configuration. A rectangular embodiment will be described in the following sections, as an example, it being understood that other shapes are contemplated within the spirit of the present invention. As will be apparent to those skilled in the art, although not shown in the figures, brackets or other linkages can be used to connect the moving coil to the load of the actuator. These brackets or other linkages can extend through longitudinal slots formed in the field blank 22 of the actuator.

20 In the embodiment of Fig. 1, permanent magnet 18 has a rectangular shape. The field blank 22 has a rectangular shape and closed ends. Permanent magnet 18 is positioned on the inside surface of the field blank and has a length which is selected so that cavities 14 and 16 are defined between the inside surfaces 20 of the ends of the field blank 22 and the permanent magnet 18. The inner dimension of permanent magnet 18 and the outer dimension of core 12 are selected so that a gap is formed between them. The moving coil 24 is constructed to be positionable in and to be moveable along this gap. Although not shown, those of ordinary skill will recognize that the moving coil 24 can be controlled through connections which extend to the exterior of field blank 22, in a conventional manner.

In the closed-ended embodiment of the present invention, compensating coils 10-B or 10-C can be positioned in one or both of the cavities 14 or 16, respectively, which have been formed between the permanent magnet 18 and the inside surfaces 20 of the field blank 22.

- 5 Alternatively, a core compensating coil 10-A can be employed which is wound around the core. The core compensating coil 10-A can be constructed to extend substantially the entire length of the core 12.

The structure provided in Fig. 1 permits the altering of the distribution of the flux density in the gap. In turn, this permits the control of the flux density as a function of the stroke. Thus, by controlling the magneto-motive force (MMF) in the compensating coils, one is able to control the characteristics of the actuator to have, for example constant force across the stroke, or other desired performance characteristic.

- 15 The open-ended embodiment of Fig. 2 is similar to that of Fig. 1, except that one end of the field blank is open.

Stationary compensating coils 10-A, 10-B and 10-C can be connected in series with the moving coil 24 in such a way that their magnetic fluxes work against magnetic flux created by current in the moving coil 24, thereby reducing armature reaction and resultant inductance, and leading to a faster response of the actuator. In this case, a new Force vs. Stroke curve would generally reflect the increased output force throughout the stroke.

- 20 However, if there is a need for a "tailored" force throughout most of the stroke, then the compensating coils should be connected to a separate power supply 26, as shown in Fig. 7. A position feedback device 28 will be used for effective control of the compensating current value as a function of stroke. Examples of such compensating current are provided in the curves depicting magneto-motive force in Ampere-turns vs. stroke for a given constant value of the output force of Fig. 3 and Fig. 4.
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Fig. 3 shows the compensating coil MMF in ampere-turns, as a function of the stroke at a constant force of 688 LB/M, for compensating coils 10-B and 10-C. Thus, for example, from Fig. 3 it can be seen that at a stroke position of  $-0.92$ , the MMF for compensating coil 10-C can be controlled to be 1000 ampere-turns so that the actuator provides a force of 688 LB/M at that point of the stroke. The MMF to be provided in the compensating coils 10-C and 10-B, can be identified from Fig. 3 in a similar manner for other moving coil positions.

Fig. 4 shows the core compensating coil MMF in ampere-turns, as a function of the stroke at a constant force of 684 LB/M, for core compensating coil 10-A. For example, from Fig. 4 it can be seen that at a stroke position of  $0.37$ , the MMF for core compensating coil 10-A can be controlled to be 1500 ampere-turns so that the actuator provides a force of 684 LB/M at that point of the stroke. The MMF to be provided in the core compensating coil 10-A, can be identified from Fig. 4 in a similar manner for other moving coil positions.

Comparison of the above curves of Figs. 3 and 4 shows that compensating coils 10-B and 10-C, located in the spaces 14 and 16 between the magnets 18 and inside walls 20 of the magnetic structure, tend to be more effective at the beginning of the stroke, whereas core compensating coils 10-A seem to widen a constant force region toward the end of the stroke considering left-to-right movement of the coil.

The Force vs. Stroke characteristics with the two different types of compensating coils are presented in Fig. 5 and Fig. 6. Fig. 5 illustrates the force vs. stroke characteristics using compensating coils such as 10-B and 10-C, while Fig. 6 illustrates the force vs. stroke characteristics using core compensating coils, such as 10-A. In Figs. 5 and 6, the curve plotting the points indicated by the diamond symbols represents the condition where the applied MMF ( $I_{cc}N_{cc}$ ) equals 0 ampere-turns (A-T). The other curves represent provided MMFs as follows:

SYMBOL	MMF (A-T)
square box	1200
"x"	3600
"x" over-striking vertical line	4800

From Fig. 5, it can be seen that as increasing MMF is provided in the compensating coils 10-B or 10-C, the force towards the end of the stroke can be increased by the compensating coils in a proportionately greater degree than the rest of the stroke. Conversely, from Fig. 6, it can be seen that the effect of core compensating coil 10-A on the force produced by the actuator is shifted toward the center of the stroke as compared to that for compensating coils 10-C or 10-B.

Depending upon a particular application, both types of the compensating coils 10-A and 10-B, 10-C can conceivably be utilized.

It should be noted that the utilization of such compensating coils increases the input power to the actuator. However, the increased dissipation occurs in the stationary coils attached to a relatively large heat sink, as opposed to a moving coil which does not have such a heat sink. Further, heat generated within a moving coil doesn't change.

The compensating coil arrangement has been described as applied to linear voice coil actuators as an example only. The same approach can be used on rotary voice coil actuators.

The terms and expressions which have been employed herein are intended as terms of description and not of limitation, and there is no intent in the use of such terms and expressions of excluding equivalents of the features shown and described, or portions thereof, it being recognized that various modifications are possible within the scope of the invention claimed.